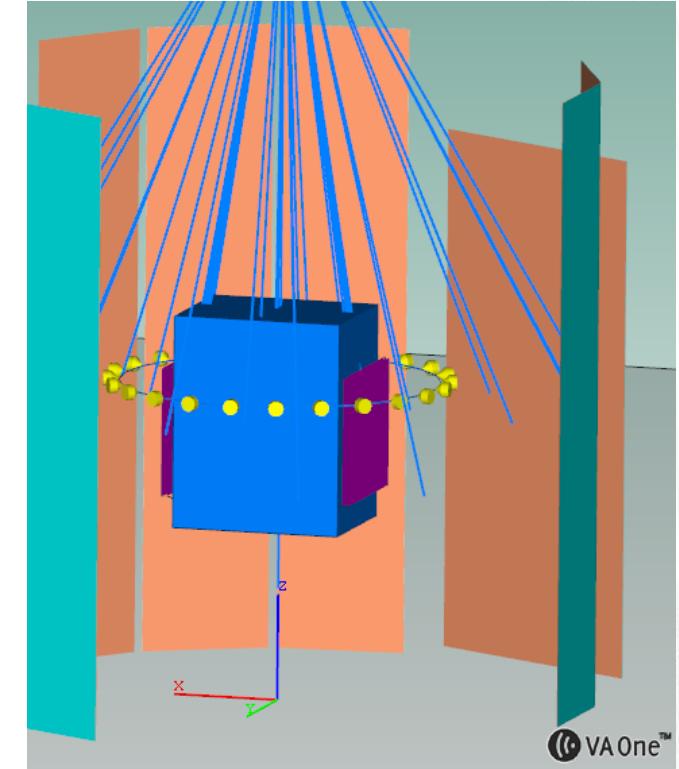
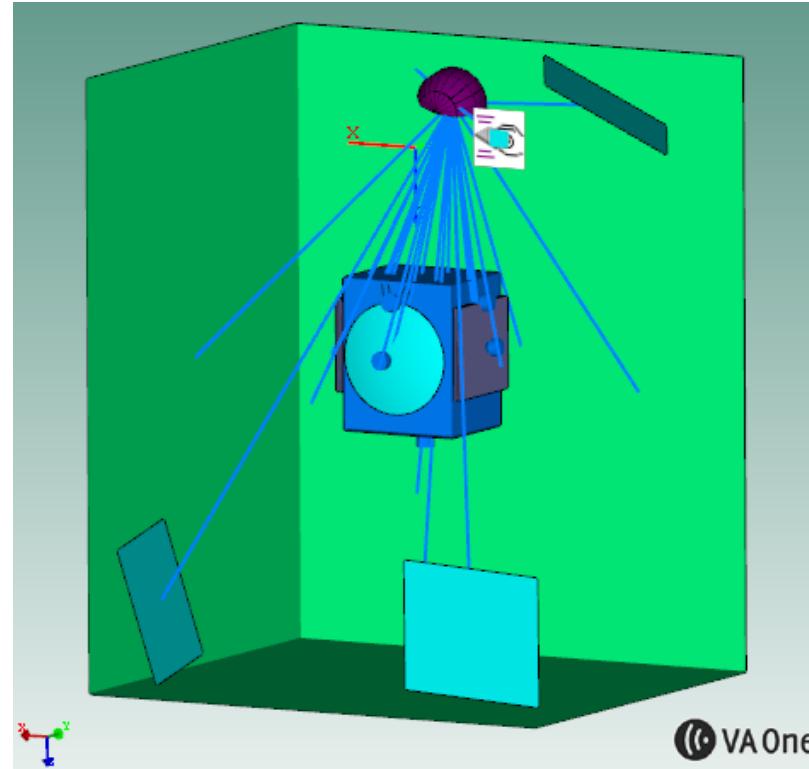
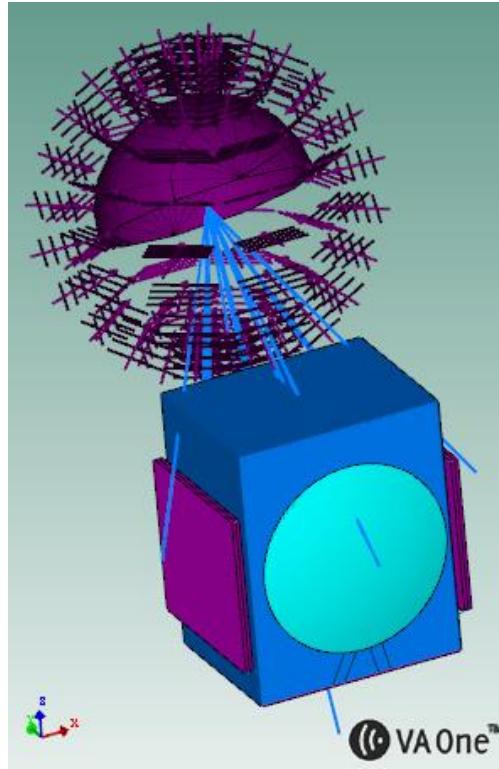


# Virtual comparison of a reverberant room, Direct Field Acoustic Test and analytical Diffuse Acoustic Field



# Agenda

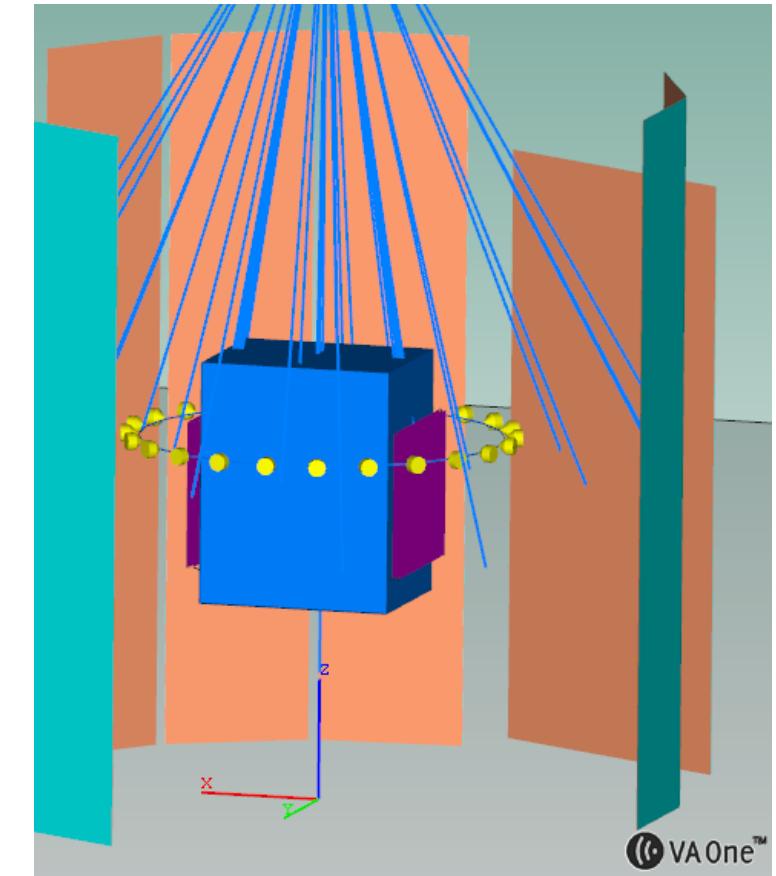
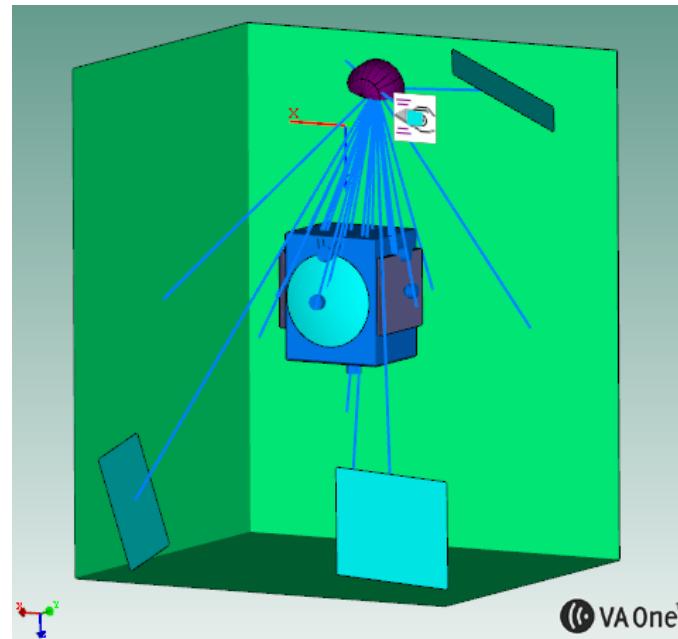
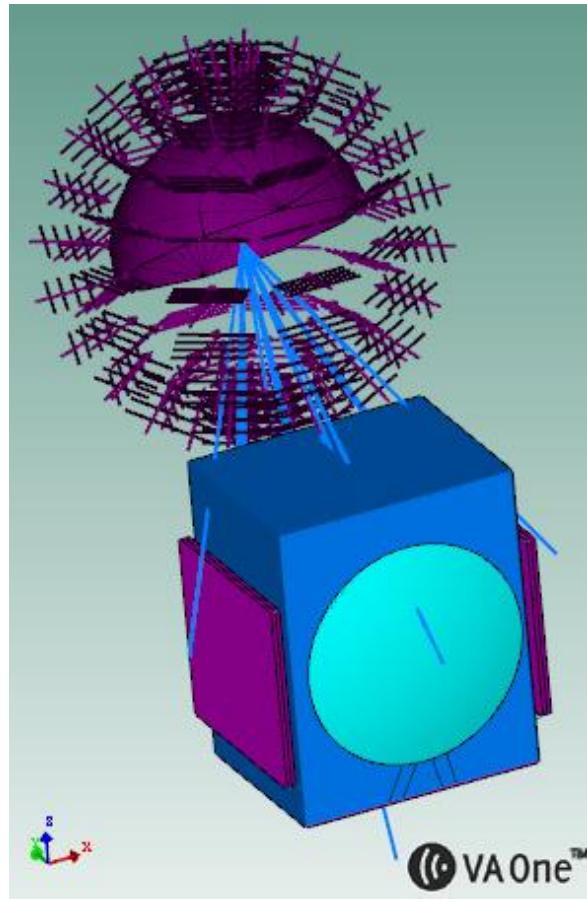
- What are we comparing?
- What can we compare?
  - Diffusivity
  - Uniformity
- Who wins the diffusivity competition?
  - Open field case
- How about uniformity?
- In the end, is it all the same?
  - Comparing the test article response
- Conclusions

# What are we comparing?

Virtual DAF

Reverberant room

DFAT setup



# Virtual DAF

## Sum of incoherent plane waves

Cross Spectral  
Pressure response

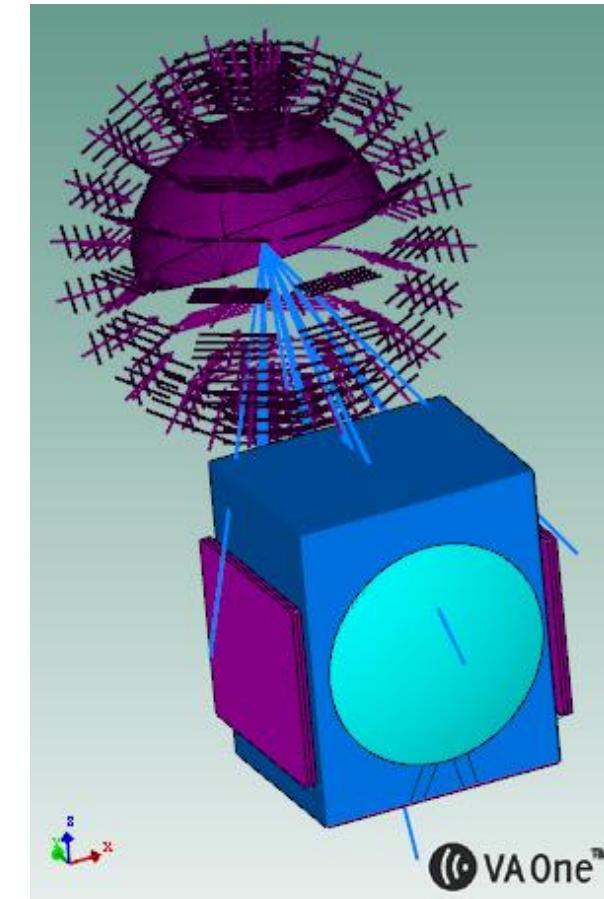
$$[S_{pp}] = [H_{pw}] [S_{ww}] [H_{pw}]^H$$

Cross Spectral Modal  
structural response

$$[S_{qq}] = [H_{qw}] [S_{ww}] [H_{qw}]^H$$

Cross Spectral Excitation  
matrix is diagonal

- Legacy method
- No Additional elements besides the structure
- Field is known to be diffuse
  - Diffusivity depends on the number of plane waves
- Represents an idealized test
  - For the actual test, it is often difficult to obtain a diffuse field in the low frequency



# Reverberant room

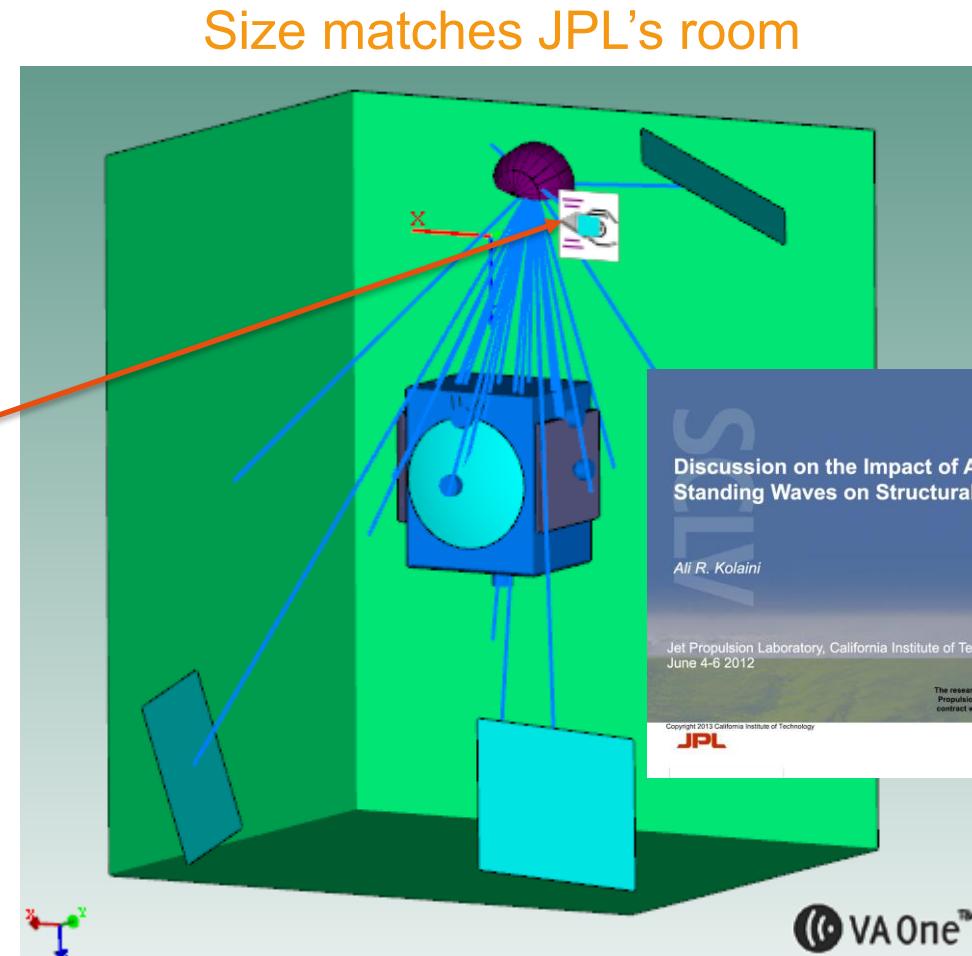
Test article is placed in a reverberant room

$$[S_{pp}] = [H_{pw}] [S_{ww}] [H_{pw}]^H$$

$$[S_{qq}] = [H_{qw}] [S_{ww}] [H_{qw}]^H$$

$[S_{ww}]$  is of size 1x1  
(single horn example)

- Represents the traditional test
- One velocity constraint is representing a horn
- A few rigid panels are introduced to break the standing waves
- Here the diffusivity is introduced by the  $[H]$  matrices as  $[S_{ww}]$  is of size 1x1



# DFAT setup

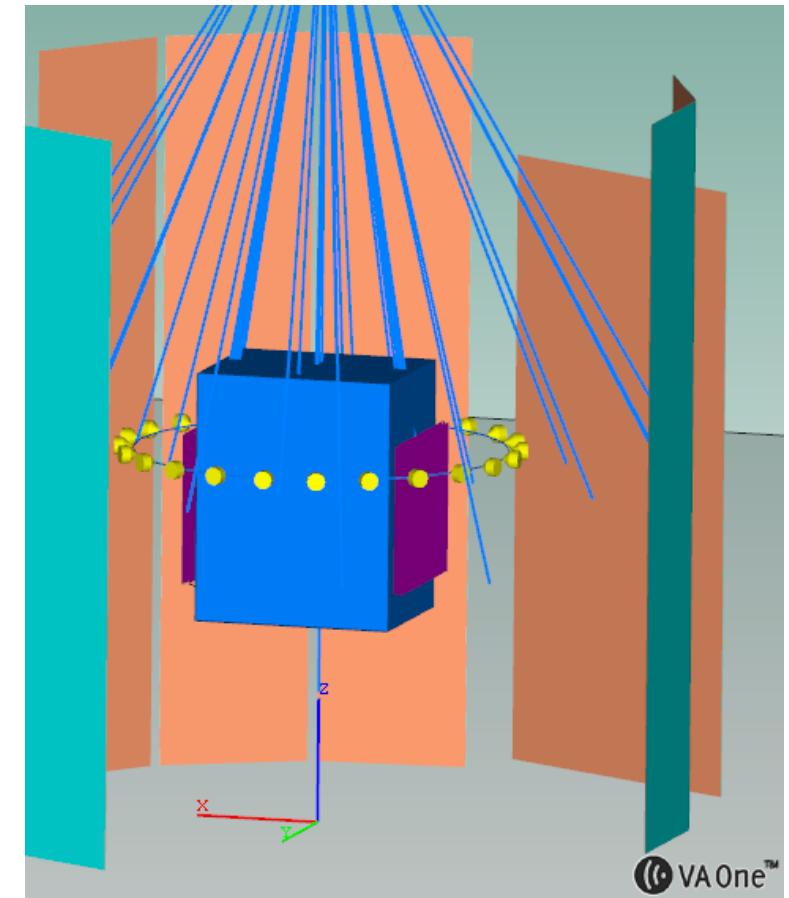
Test article is excited with stacks of speakers and a control loop

$$[S_{pp}] = [H_{pw}][S_{ww}][H_{pw}]^H$$

$$[S_{qq}] = [H_{qw}][S_{ww}][H_{qw}]^H$$

Cross Spectral Excitation matrix is  $n_{\text{stacks}}$  x  $n_{\text{stacks}}$  and is optimized to have a diffuse field at the control microphones

- New testing method
- Speaker stacks are represented by faces with constraints at their surface
  - Measured impedance is placed at the stack surface
  - Here each stack is correlated but alternative configurations can be studied
- Ground is modeled with an infinite rigid plane



# DFAT setup

Test article is excited with stacks of speakers and a control loop

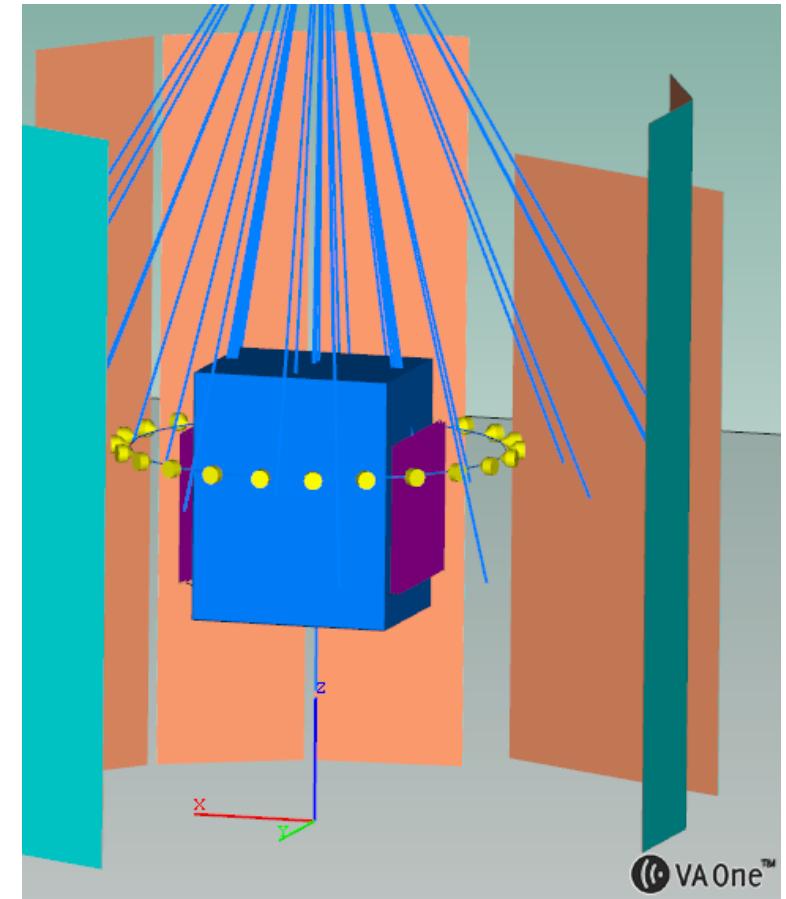
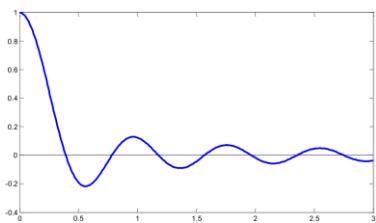
$$[S_{pp}] = [H_{pw}][S_{ww}][H_{pw}]^H$$

$$[S_{qq}] = [H_{qw}][S_{ww}][H_{qw}]^H$$

Cross Spectral Excitation matrix is  $n_{\text{stacks}}$  x  $n_{\text{stacks}}$  and is optimized to have a diffuse field at the control microphones

- $[S_{ww}]$  is optimized using pseudo inverse of  $[H_{pw}]$  for an ideal  $[S_{pp}]_{\text{Control\_Mic}}$  based on the control microphone locations
  - $[S_{pp}]_{\text{Control\_Mic}}$  can be obtained based on the known cross correlation of a diffuse acoustic field between any two known control microphones

$$S_{pp}(r) = A \frac{\sin(k_0 r)}{k_0 r}$$



## Additional “complicating” effects

- Stacks are made of subwoofers and mid-frequency speakers
  - Terms of  $[H_{pw}]$  and  $[H_{nw}]$  are then null when speakers do not output power
  - Here subwoofers output power up to 240Hz
  - Mid-frequency speakers do not output power below 200Hz
- f < 200 Hz, 6 active stacks
- f > 200 Hz & f < 240 Hz, 15 active stacks
- f > 240 Hz, 9 active stacks
- Certain speakers may be correlated with each other
  - Introduction of a control matrix defining which speakers are correlated with each other
  - For this example, all speakers within stack are correlated
- MSI uses a proprietary Matrix Switch that combines drives
  - This can be accounted for
  - For this study, 24 control microphones are placed around the tested structure (no Matrix switch)

# What can we compare?

## Uniformity

- Pressure field amplitude is expected to be uniform
  - A reverberant room is expected to show less than 1.5dB of pressure standard deviation
- Simulation can recover a lot of pressure information
  - We can easily quantify the pressure standard deviation



In the 3<sup>rd</sup> Octave band!

# What can we compare?

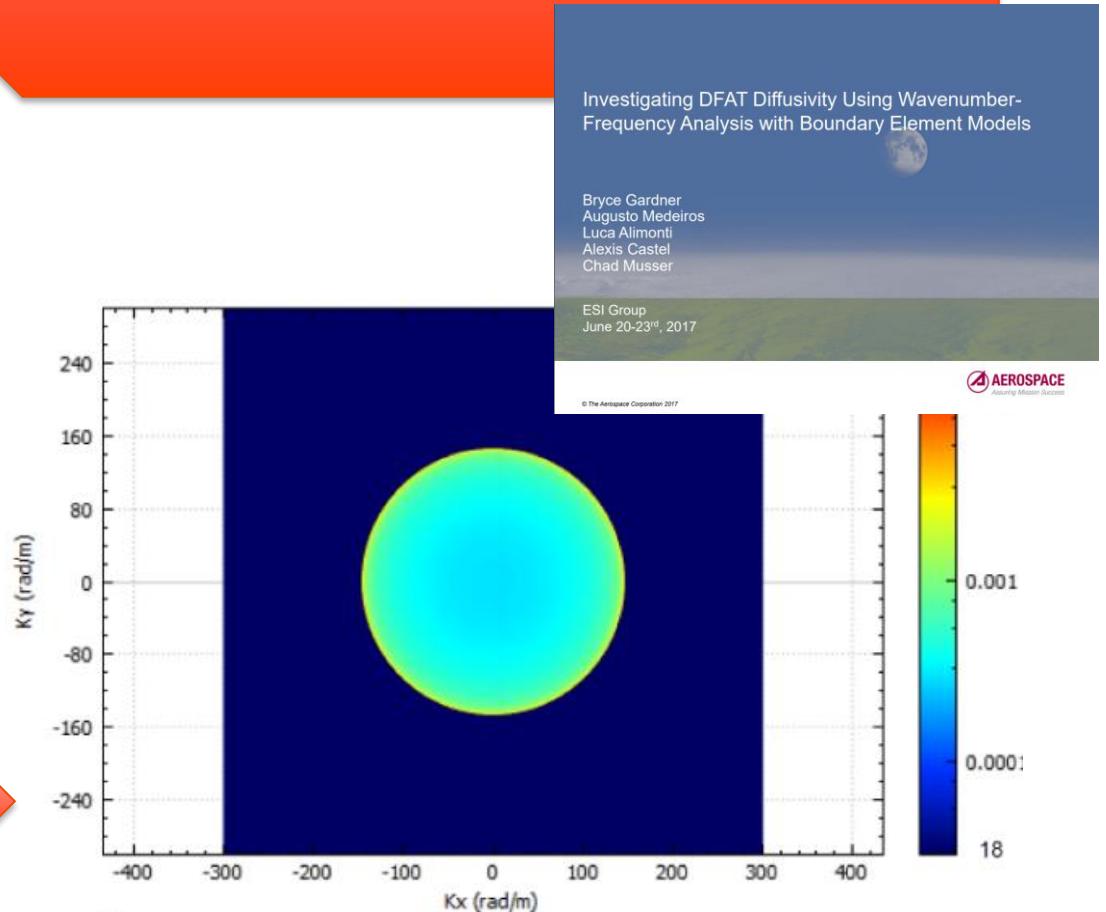
## Diffusivity

- $[S_{pp}]$  is known for all data recovery faces
  - Defines the cross-correlation between any two nodes where the pressure is recovered
  - $[S_{pp}]$  is known for a Diffuse Acoustic Field (DAF) but is difficult to visualize
  - The corresponding Wavenumber-Frequency spectrum can also be calculated

$$S_{pp}(\mathbf{k}, \omega) = \text{FFT}([S_{pp}(\mathbf{x}, \omega)])$$

- For a DAF,  $S_{pp}(\mathbf{k}, \omega) = \frac{2\pi}{k_0^2} \frac{1}{\sqrt{1-|\mathbf{k}|^2/k_0^2}}, |\mathbf{k}| < k_0$

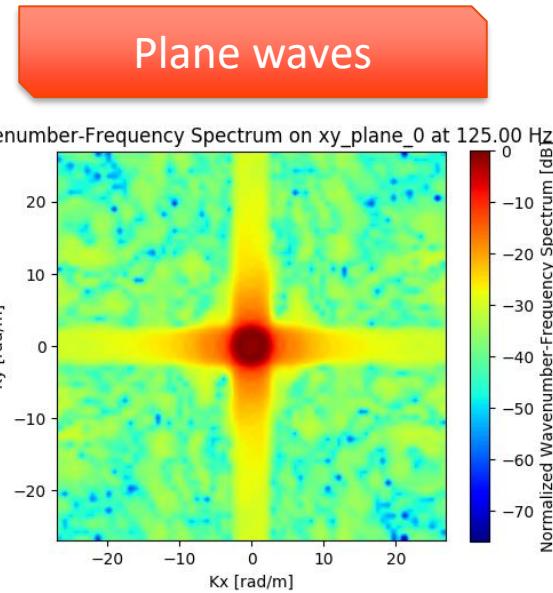
One can then evaluate the field diffusivity by comparing the simulated  $S_{pp}(\mathbf{k}, \omega)$  to its analytical form for a DAF



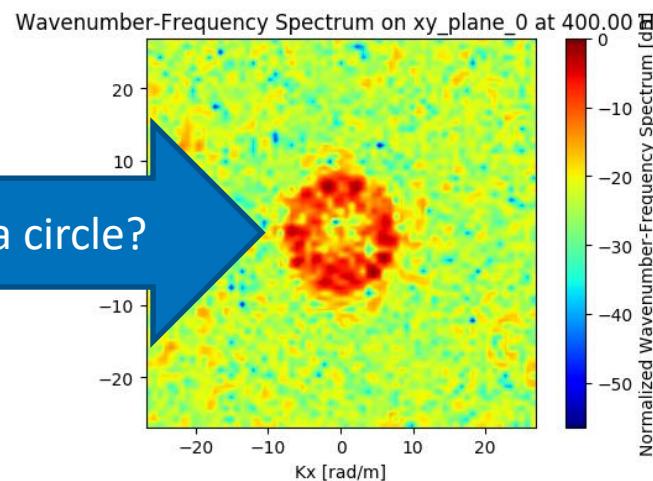
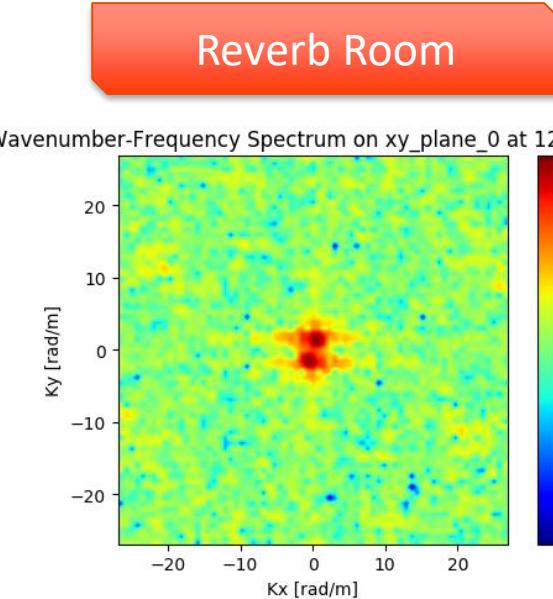
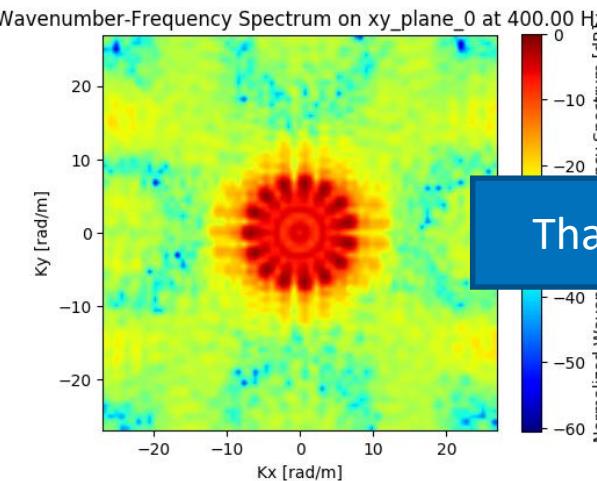
# Who wins the diffusivity competition?

## Open field study

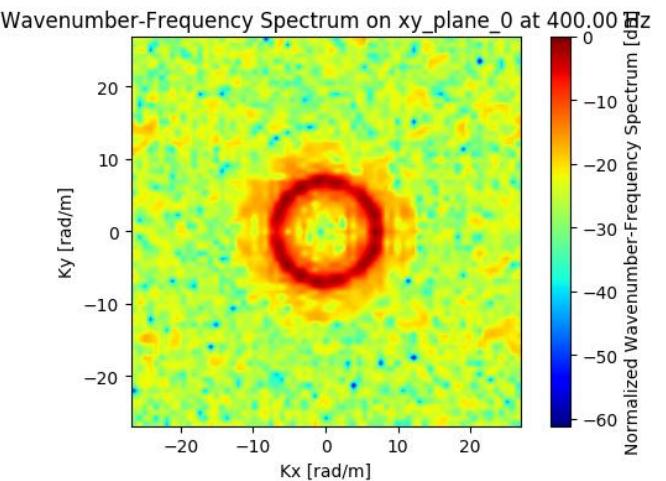
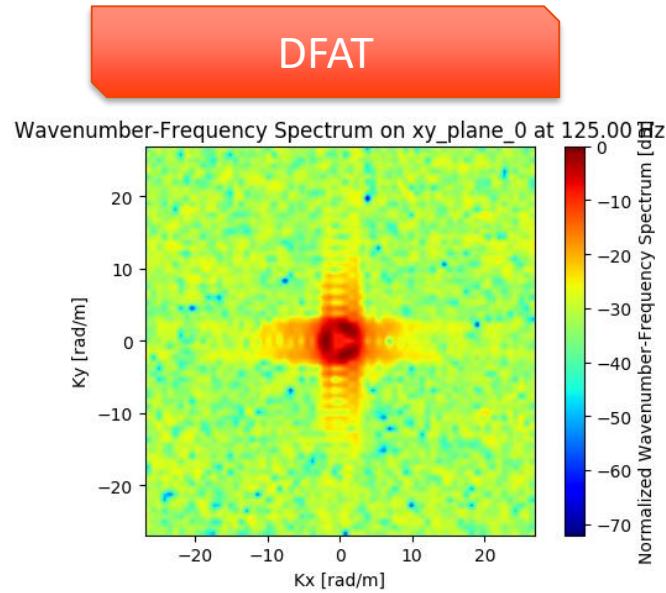
125 Hz



400 Hz

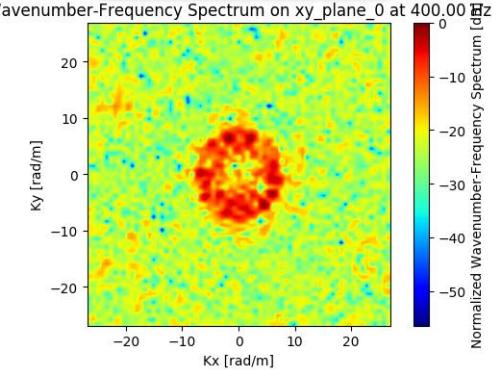


That's a circle?

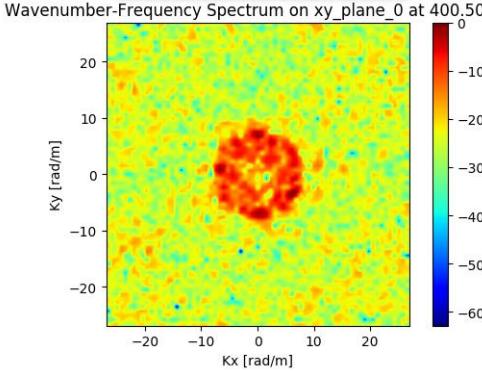


# What's happening in the reverb room?

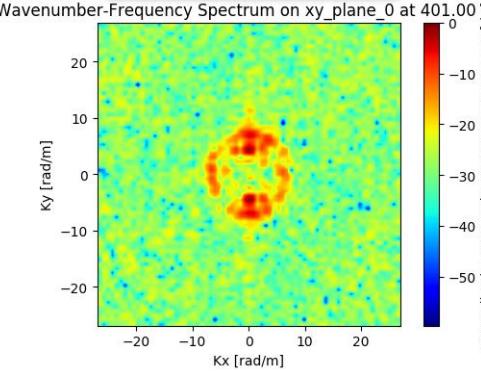
400.0Hz



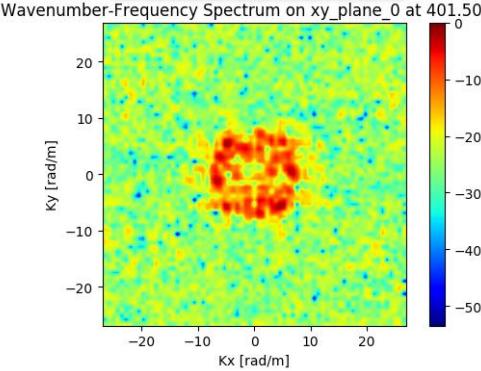
400.5Hz



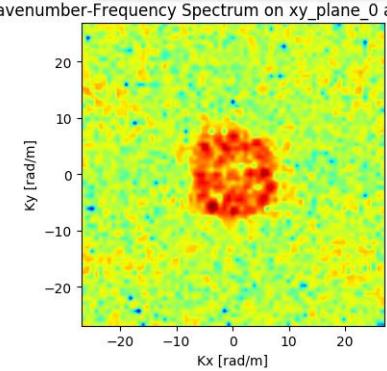
401.0Hz



401.5Hz

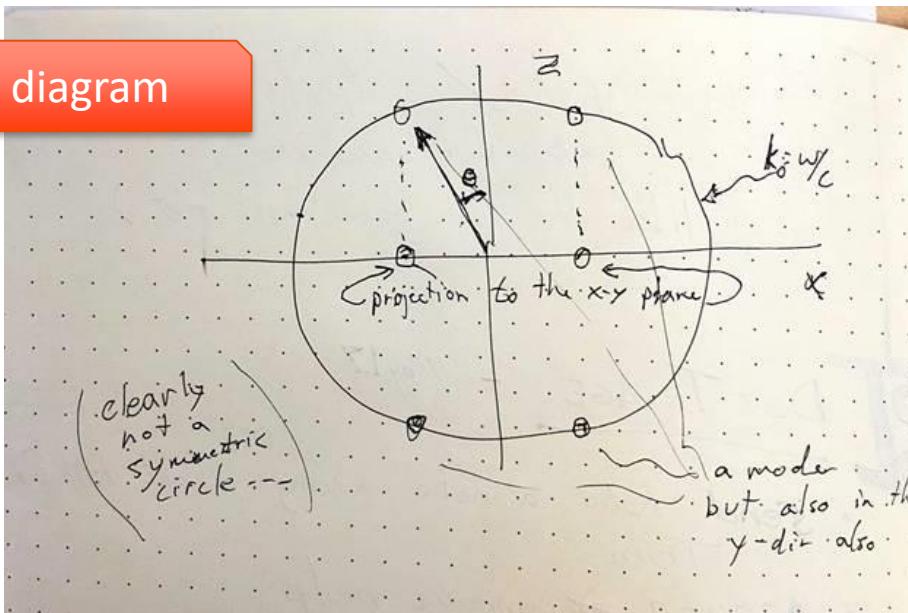


402.0Hz



- Each discrete frequency does not seem diffuse

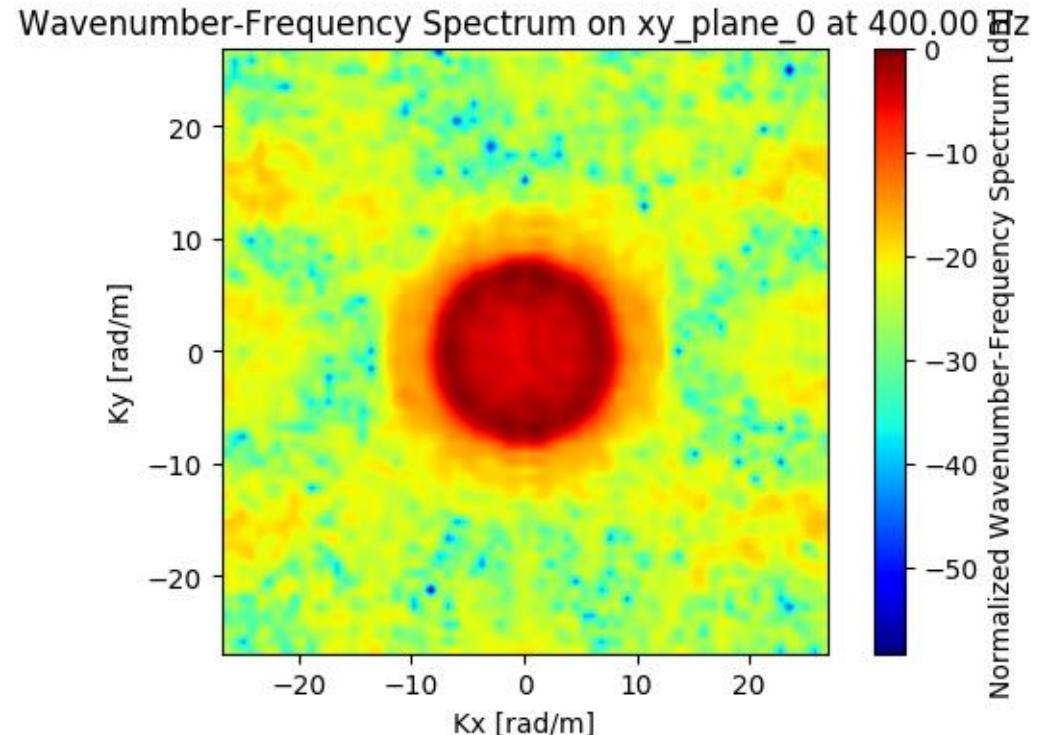
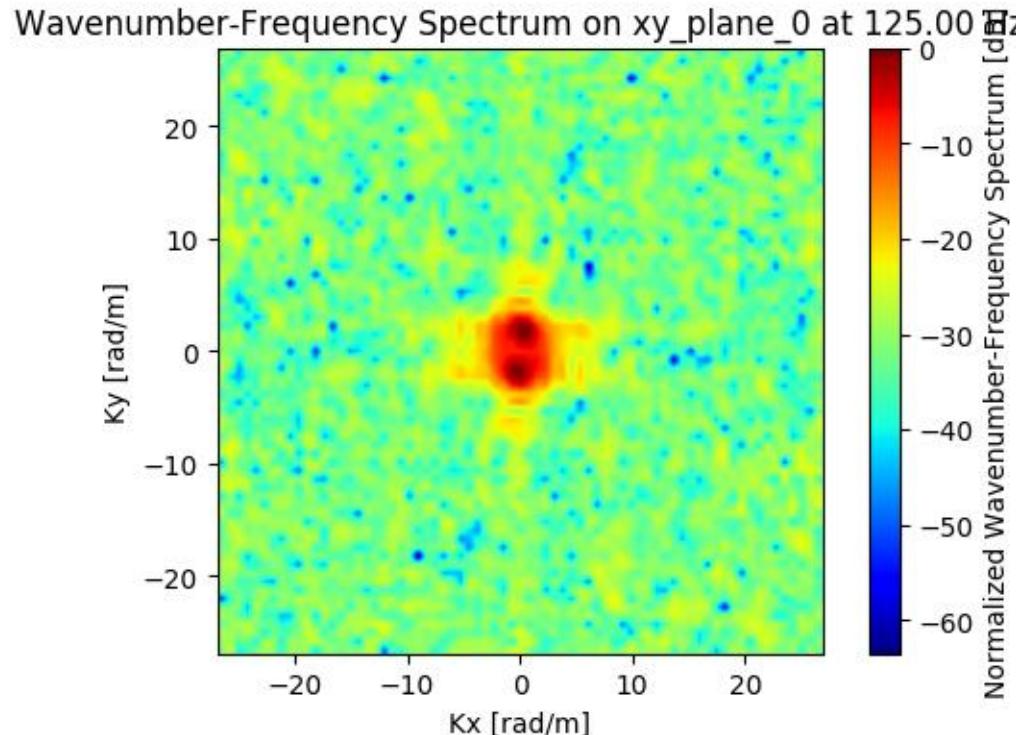
Bryce's diagram



Individual modes are projected on the data recovery and form high intensity regions at discrete frequencies

# What's happening in the reverb room?

- Looking at the WFS in the third Octave band



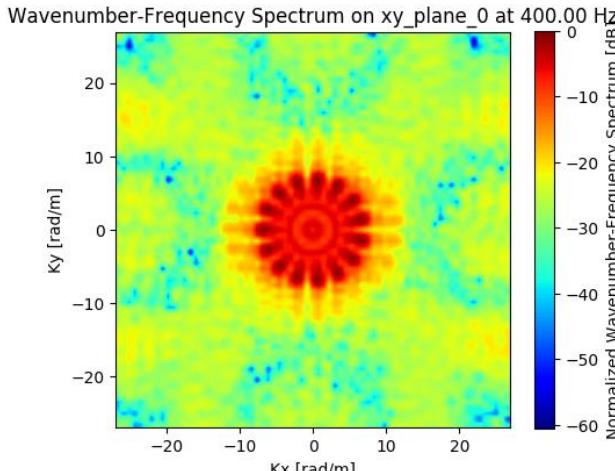
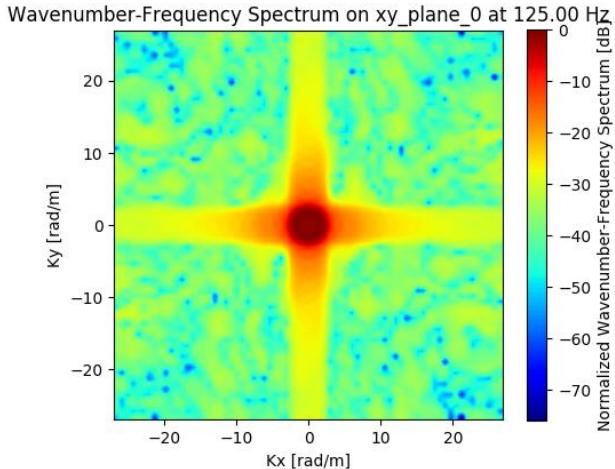
The room has indeed a diffuse field in the high frequency!

# Who wins the diffusivity competition?

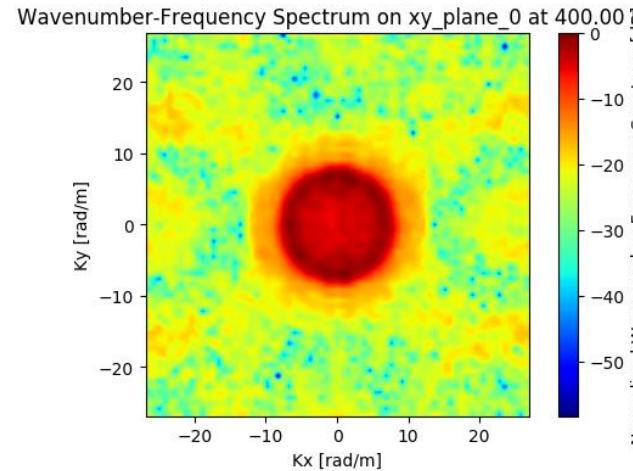
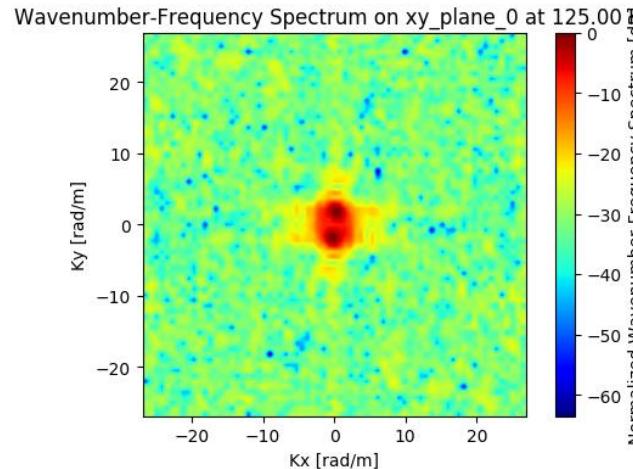
## Open field study

3<sup>rd</sup> Octave band results

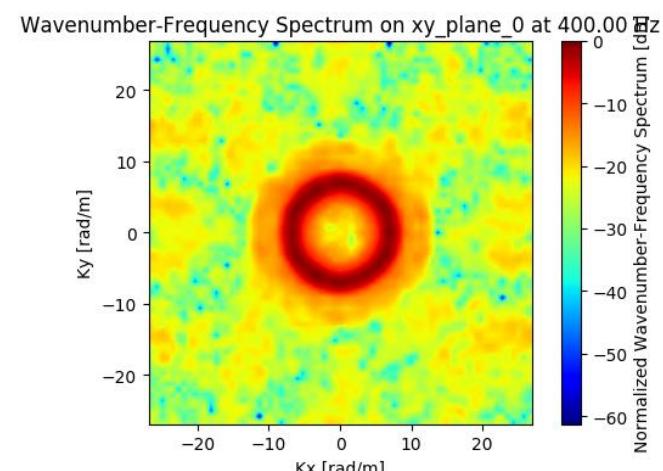
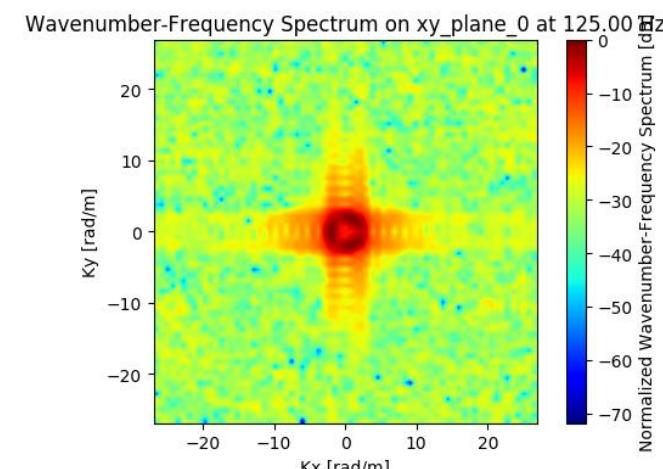
Plane waves



Reverb Room



DFAT



125 Hz

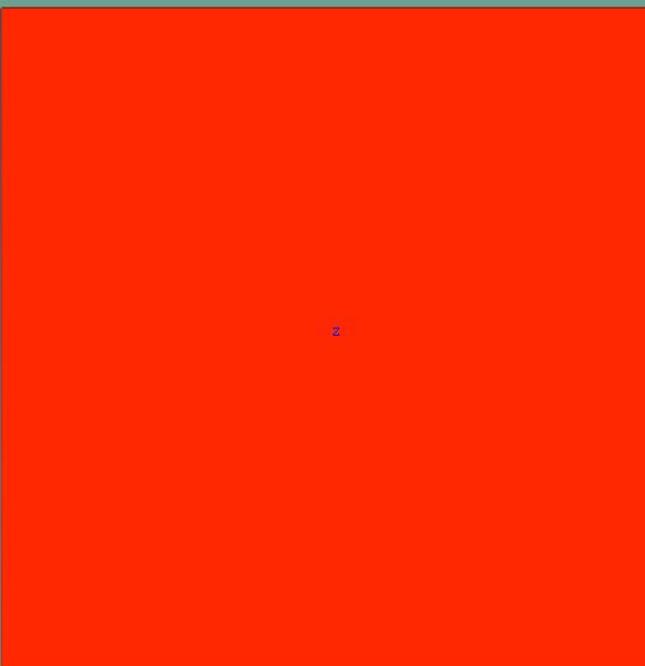
400 Hz

# How about uniformity?

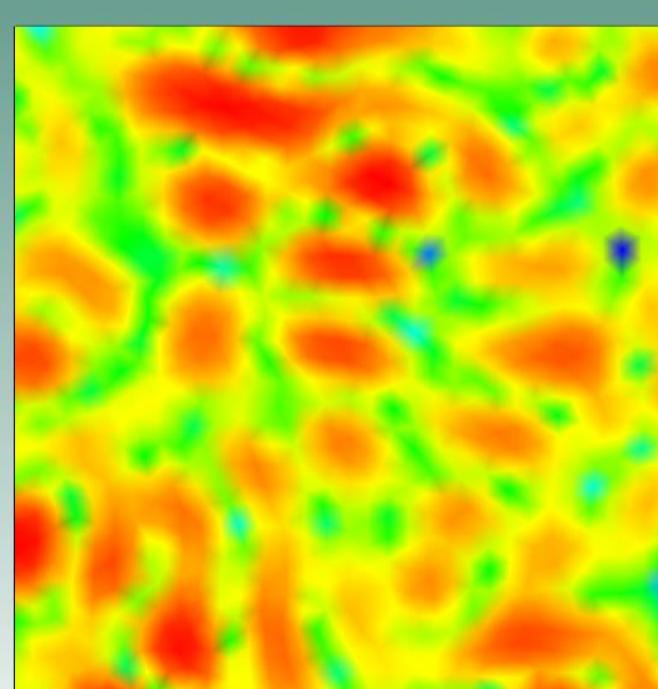
## Discrete Frequency Contour

Narrow band results

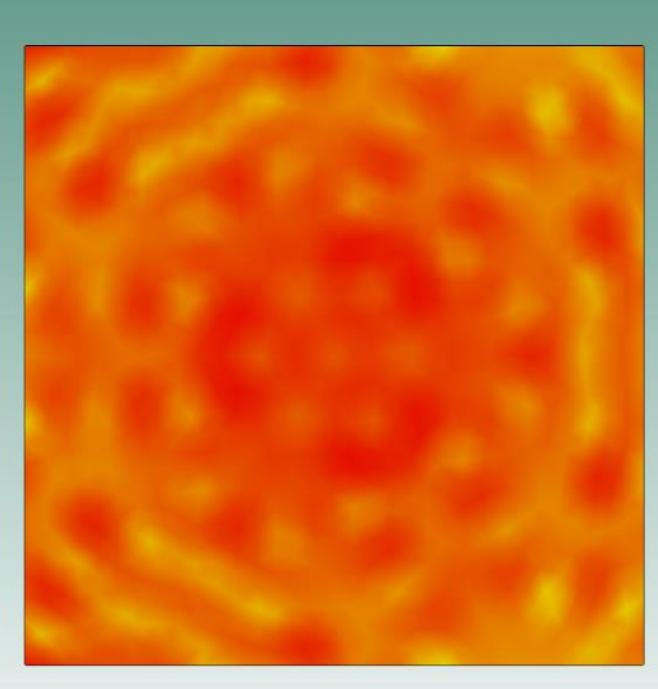
Plane waves



Reverb Room



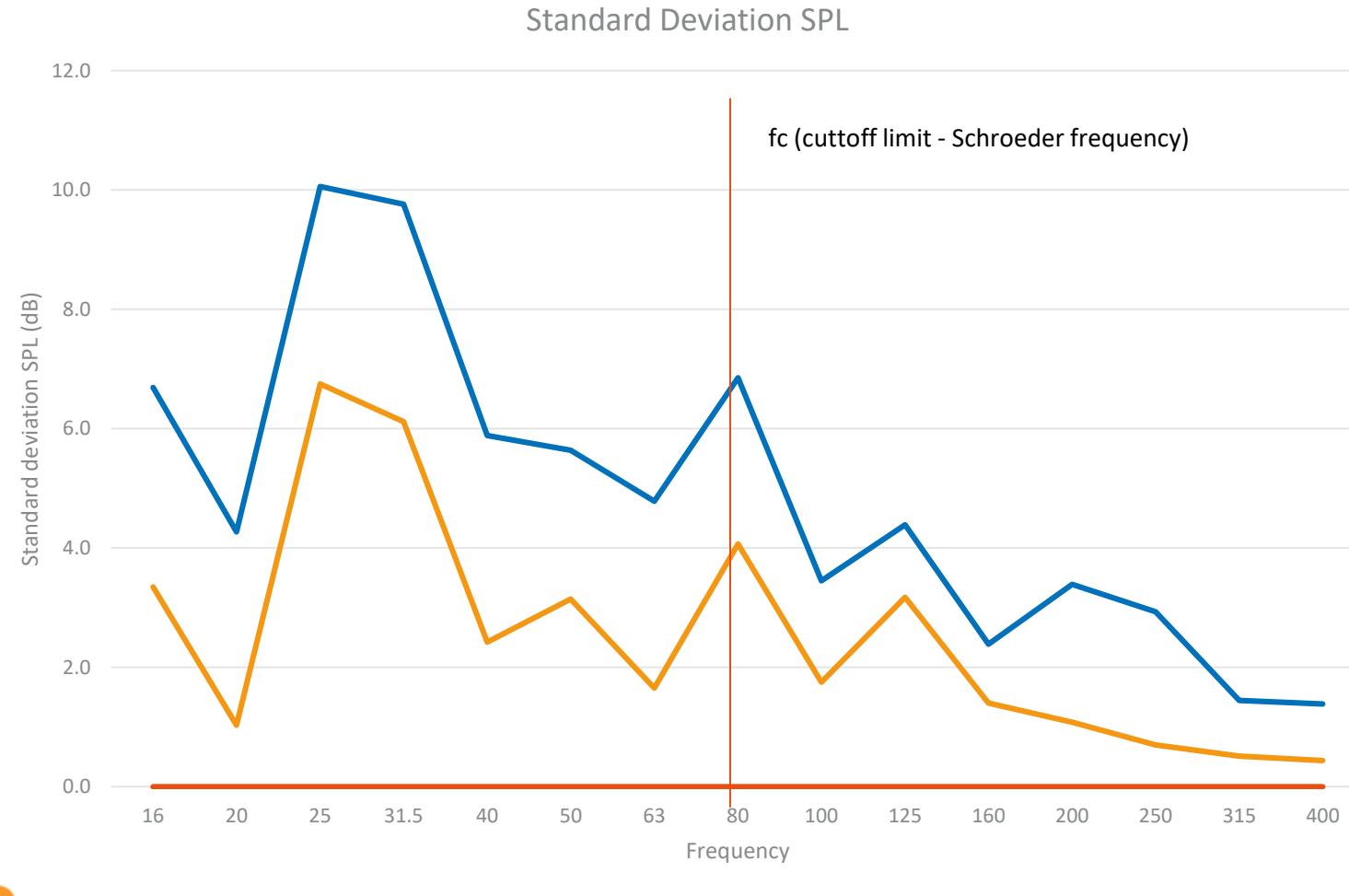
DFAT



# How about uniformity?

## 3<sup>rd</sup> Octave Standard deviation

### 3<sup>rd</sup> Octave band results



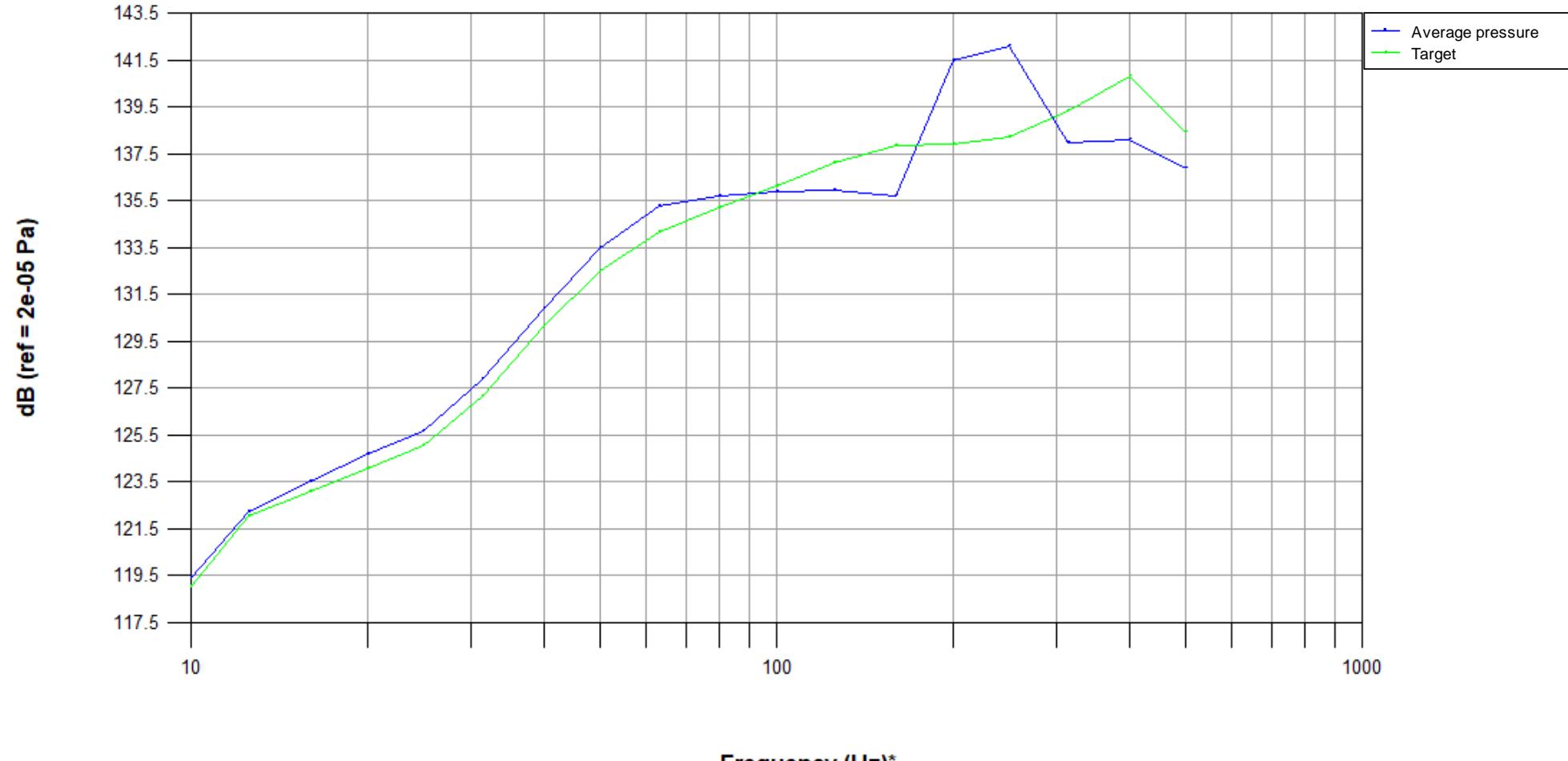
Again, we can't look at the field uniformity for a single discrete frequency.

Data needs to be converted to the 3<sup>rd</sup> Octave band.

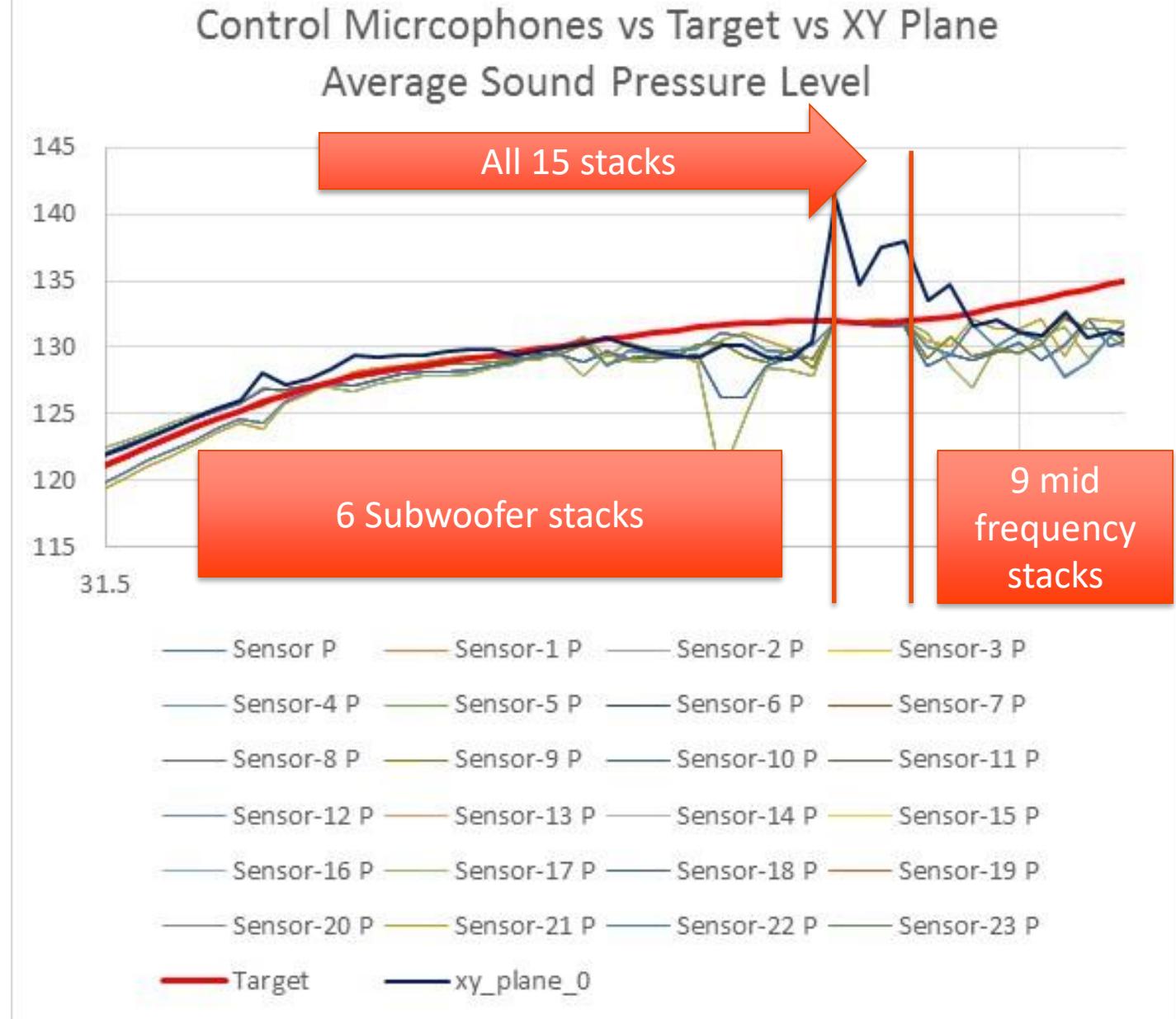
# DFAT Average Plane Pressure vs Target

3<sup>rd</sup> Octave band results

Engineering Units

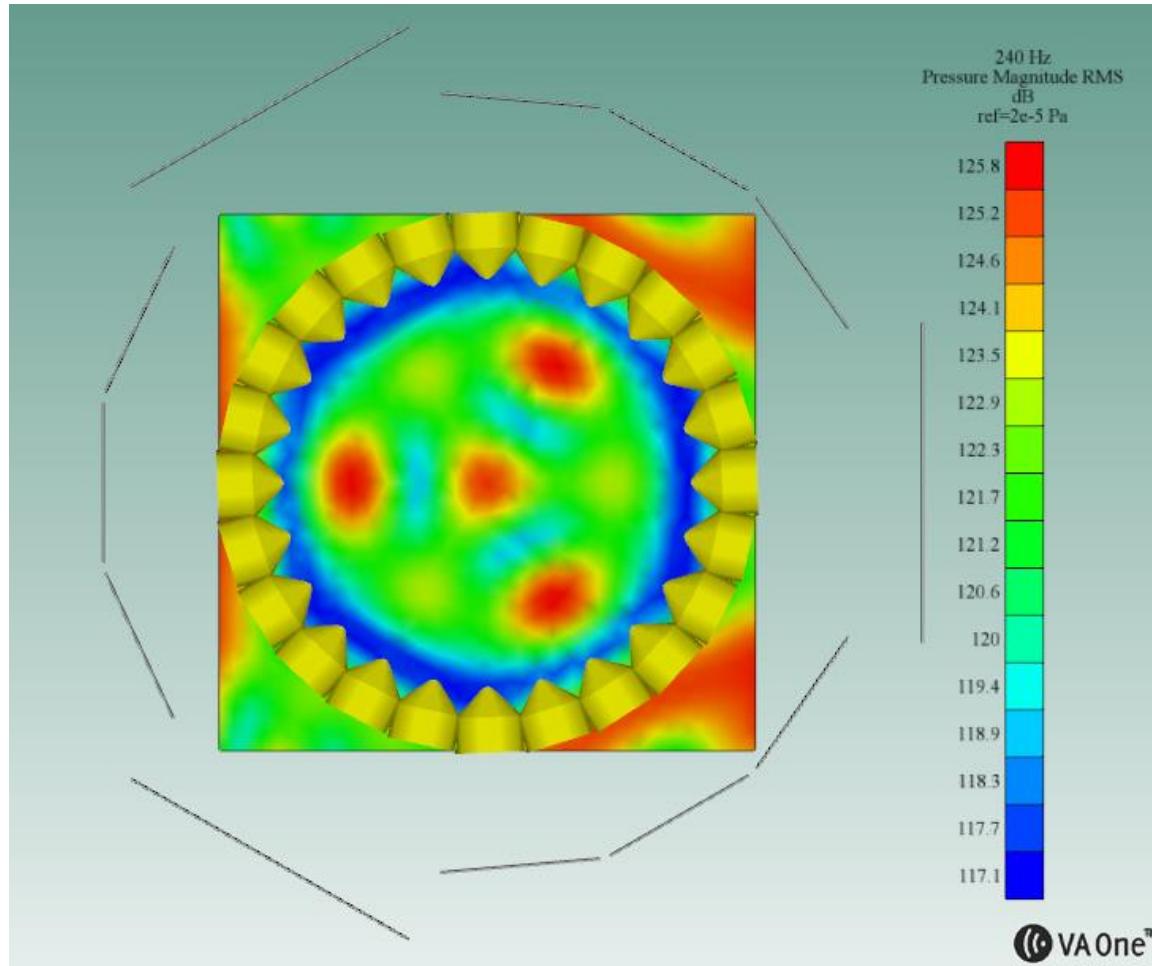


- Control microphones do not exceed the target level
- Levels are better matched when the number of stacks is greater



# Looking at the contour plot

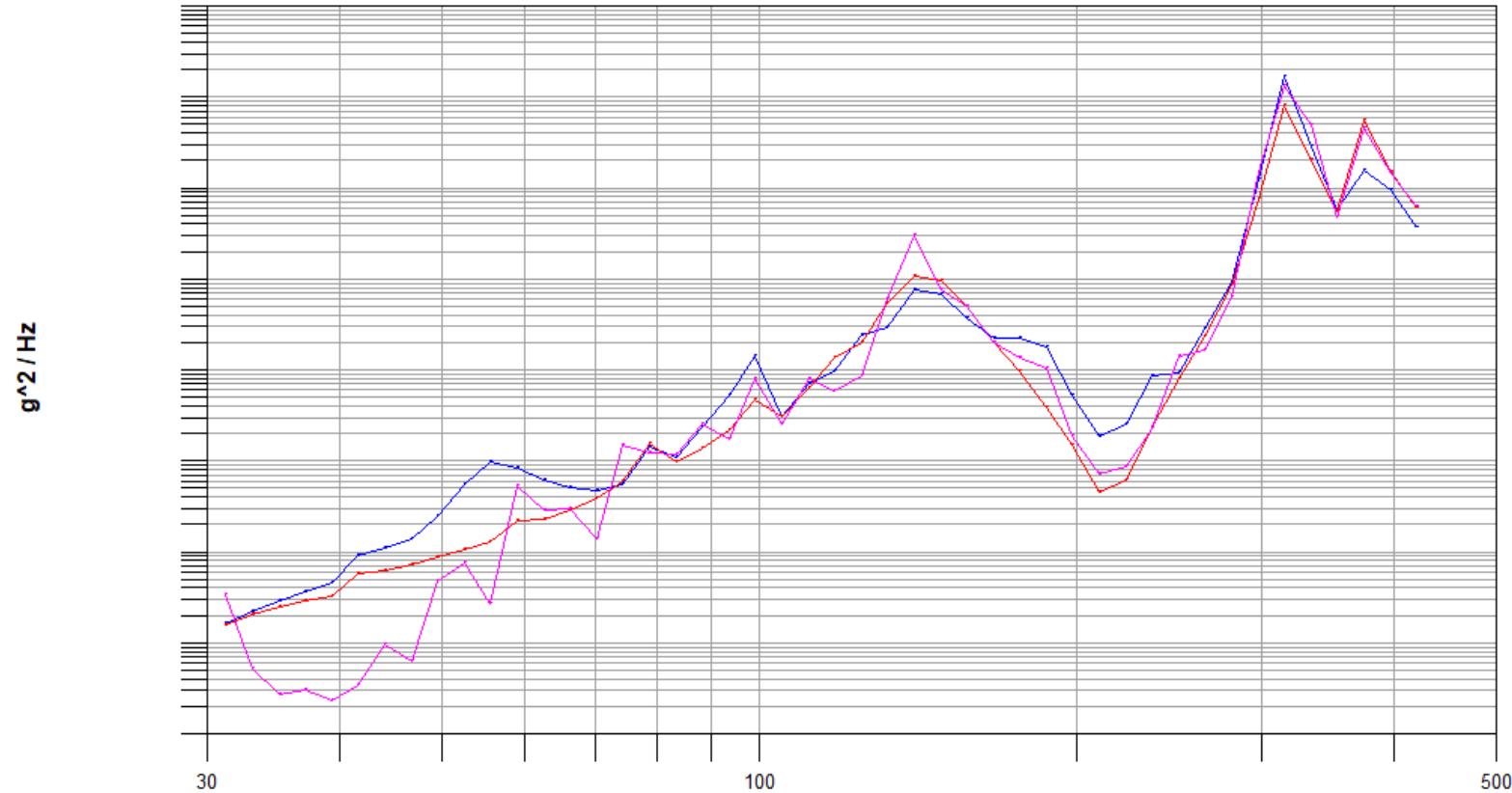
- Average SPL on the plane may not be ideal
  - Too large
  - Receives direct field from speaker
- After discussing with MSI, having the spacecraft present helps eliminating hot spots within the circle



# In the end, is it all the same? Structural response comparison

Guess which is DFAT?

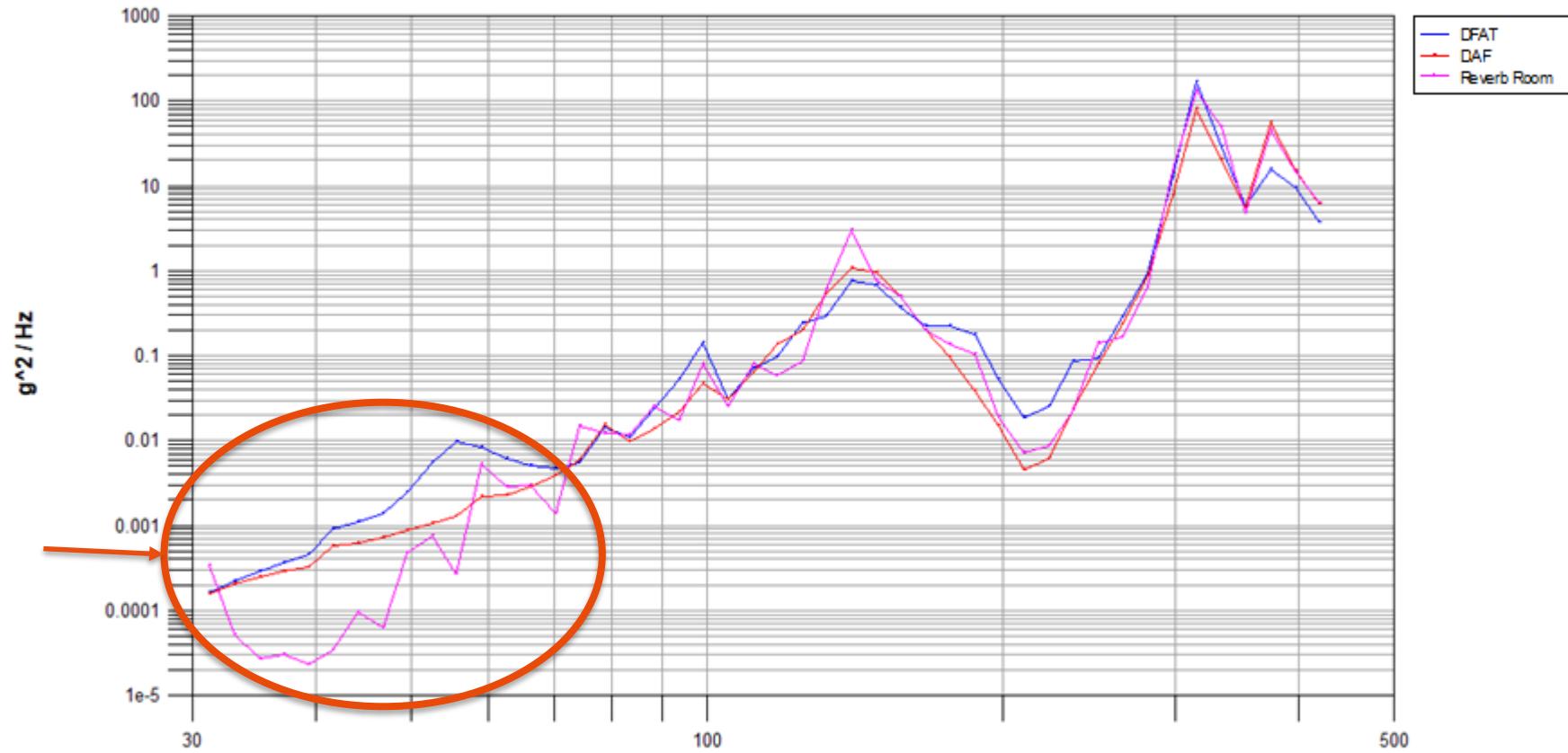
Acceleration Sensor Response-Reflector Center Sensor



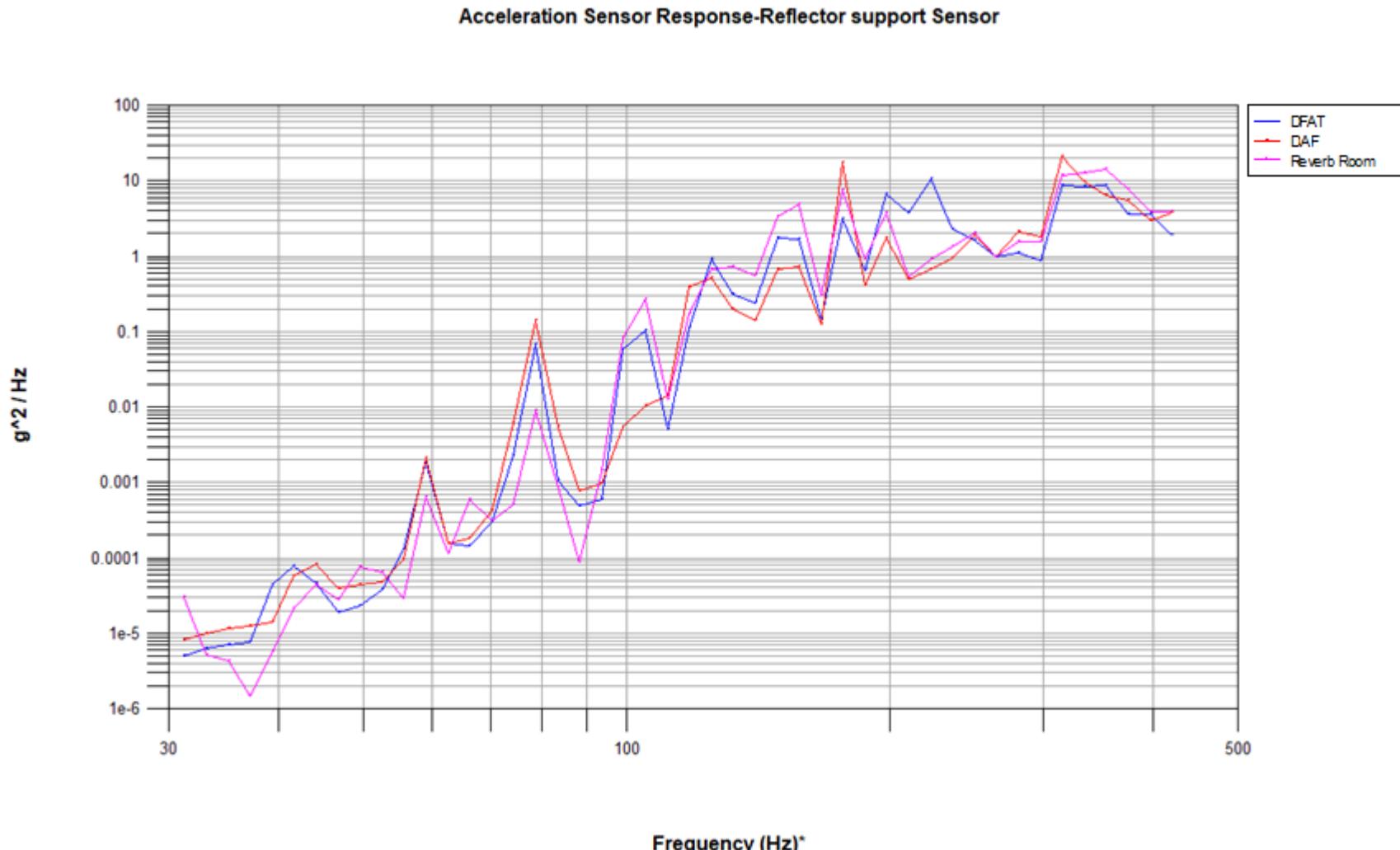
# In the end, is it all the same? Structural response comparison

## Solution

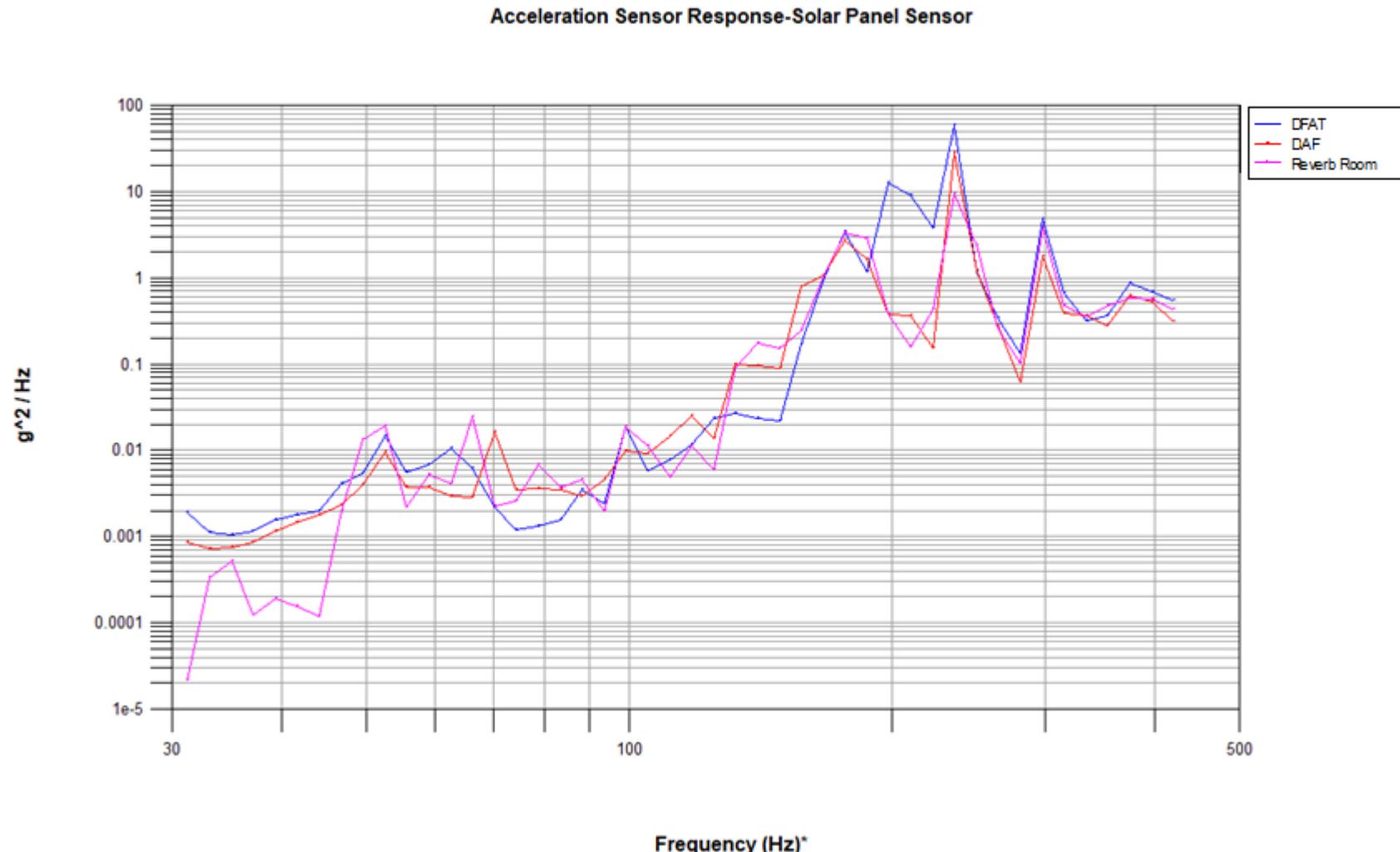
Acceleration Sensor Response-Reflector Center Sensor



# In the end, is it all the same? Structural response comparison



# In the end, is it all the same? Structural response comparison



# Conclusions

- Simulation processes are available to simulate diffuse acoustic field excitations
  - DFAT simulation process is now available
- Simulating analytic DAF vs simulating the test shows major differences
  - Reverberant room is only exhibiting DAF properties
    - In the high frequency range (>160 Hz for the simulated case)
    - When looking at specifications in the third octave band
  - DFAT field is more diffuse and more uniform at discrete frequencies
  - Reverb room is still diffuse and uniform when the results are in the third octave band
- Once a test article is present, the field is more uniform and it is hard to distinguish responses from any of the three simulation methods
- Next step
  - Correlation study of DFAT test data
  - Using simulation to optimize the physical test

